

Amendments to the Claims:

This listing of claims will replace all prior versions and listings of claims in the application.

1. (currently amended) A dry premix for preparing a pourable mortar with a high degree of fluidity comprising a hydraulic binder, finely ground slag, a fluidifier and/or superfluidifier, a setting regulator, and aggregates, wherein characterized as follows:

- (i) the aggregates are made up, for 75-95 wt % of the aggregates are made, of three highly monogranular fractions (A, B, C), having a characteristic grain diameter increasing progressively from A to B to C;[[.]]
- (ii) the ratio between the characteristic grain diameters of the fractions C and B is comprised between 2.2 and 3.2;
- (iii) the ratio between the characteristic grain diameters of the fractions B and A is comprised between 2.2 and 3.2;
- (iv) the remaining 5-25 wt % portion of aggregates (5-25 wt %) consists of a fourth fraction (D) having a low lower monogranularity than fractions A, B, C, and a characteristic grain diameter not lower than 0.1 mm; and
- (v) Fraction fraction A represents consists of at least 40 wt % of the total aggregates present in the dry premix.

2. (original) The premix according to claim 1, where the ratio between the characteristic grain diameters of the fractions C/B and/or B/A is comprised between 2.5 and 3.0.

3. (previously presented) The premix according to claim 1, wherein the fractions A, B, C represent 85-92 wt % of the total aggregates, and the fraction D represents 8-15 wt % of the total aggregates.

4. (previously presented) The premix according to claim 1, wherein the division in weight percentage of the three fractions A, B, C, with respect to their sum, is the following:

- Fraction A: 50 wt %-70 wt %;
- Fraction B: 10 wt %-20 wt %;
- Fraction C: 18 wt %-32 wt %.

5. (previously presented) The premix according to claim 1, wherein the division in weight percentage of the three fractions A, B, C, with respect to their sum, is the following:

- Fraction A: 55 wt %-65 wt %;
- Fraction B: 12 wt %-18 wt %;
- Fraction C: 21 wt %-29 wt %.

6. (currently amended) The premix according to claim 1, wherein the characteristic grain diameter X_0 of the different fractions of aggregates is the following:

- Fraction A: 0.2-0.4 mm;
- Fraction B: 0.6-0.8 mm;
- Fraction C: 1.6-2.4 mm;

Fraction D: 0.1-0.3 mm.

7. (previously presented) The premix according to claim 1, where the aggregates as a whole represent from 40 wt % to 60 wt % of the dry premix.
8. (previously presented) The premix according to claim 1, where the hydraulic binder is a Portland cement.
9. (currently amended) The premix according to claim 1, where the fluidifiers/superfluidifiers are ~~compounds selected from the group consisting of~~ a melaminic, naphthalenic, ~~or and~~ acrylic-type ~~compounds~~.
10. (previously presented) The premix according to claim 1, where the setting regulators are citric acid, boric acid, and tartaric acid.
11. (currently amended) A pourable cementitious mortar comprising water, a hydraulic binder, finely ground slag, a fluidifier and/or superfluidifier, a setting regulator, and aggregates, characterized as follows:
 - (i) the aggregates are made up, for 75-95 wt %, of three highly monogranular fractions (A, B, C) having a characteristic grain diameter increasing progressively from A to B to C;[[.]]
 - (ii) the ratio between the characteristic grain diameters of the fractions C and B is comprised between 2.2 and 3.2;
 - (iii) the ratio between the characteristic grain diameters of the fractions B and A is comprised between 2.2 and 3.2;

- (iv) the remaining 5-25 wt % portion of aggregates ~~(5-25 wt %)~~ consists of a fourth fraction {D} having a low lower monogranularity than fractions A, B, C; and
- (v) fraction A represents at least 40 wt % of the total aggregates present in the mortar.

12. (canceled)

13. (currently amended) A method of using a pourable mortar comprising water, a hydraulic binder, finely ground slag, a fluidifier and/or superfluidifier, a setting regulator, and aggregates, characterized as follows:

- (i) the aggregates are made up, for 75-95 wt %, of three highly monogranular fractions {A, B, C} having a characteristic grain diameter increasing progressively from A to B to C;[[.]]
- (ii) the ratio between the characteristic grain diameters of the fractions C and B is comprised between 2.2 and 3.2;
- (iii) the ratio between the characteristic grain diameters of the fractions B and A is comprised between 2.2 and 3.2;
- (iv) the remaining 5-25 wt % portion of aggregates ~~(5-25 wt %)~~ consists of a fourth fraction {D} having a low lower monogranularity than fractions A, B, C; and
- (v) fraction A represents at least 40 wt % of the total aggregates present in the mortar, for applications in the cement sector.

14. (previously presented) The method according to claim 13, for the recovery of deteriorated building works, consolidation of rock formations, structural reinforcement, injection in the conduits of tendons, immobilization of toxic-noxious refuse, and in the production of cementitious products by means of pouring in moulds.

15. (previously presented) The method according to claim 14, in which said moulds are foundry earth moulds.

16. (currently amended) A process for preparing a pourable mortar with a high degree of fluidity, said process comprising mixing together water and a hydraulic binder, finely ground slag, a fluidifier and/or superfluidifier, a setting regulator, and aggregates characterized as follows:

- (i) the aggregates are made up, for 75-95 wt %, of three highly monogranular fractions (A, B, C), having a characteristic grain diameter increasing progressively from A to B to C;
- (ii) the ratio between the characteristic grain diameters of the fractions C and B is comprised between 2.2 and 3.2;
- (iii) the ratio between the characteristic grain diameters of the fractions B and A is comprised between 2.2 and 3.2;
- (iv) the remaining 5-25 wt % portion of aggregates (5-25 wt %) consists of a fourth fraction (D) having a low lower monogranularity than fractions A, B, C; and
- (v) fraction A represents at least 40 wt % of the total aggregates present in the dry premix.

17. (previously presented) The process for preparing cementitious products, characterized by pouring and solidifying in appropriate moulds a mortar according to claim 11.

18. (previously presented) A cementitious product obtainable by means of the process described in claim 16.

19. (currently amended) The cementitious product comprising a hydraulic binder, finely ground slag, a fluidifier and/or superfluidifier, a setting regulator, and aggregates characterized as follows:

- (i) the aggregates are made up, for 75-95 wt %, of three highly monogranular fractions (A, B, C), having a characteristic grain diameter increasing progressively from A to B to C;
- (ii) the ratio between the characteristic grain diameters of the fractions C and B is comprised between 2.2 and 3.2;
- (iii) the ratio between the characteristic grain diameters of the fractions B and A is comprised between 2.2 and 3.2;
- (iv) the remaining 5-25 wt % portion of aggregates (5-25 wt %) consists of a fourth fraction (D) having a low lower monogranularity than fractions A, B, C; and
- (v) fraction A represents at least 40 wt % of the total aggregates present in the dry premix.

20. (currently amended) A cementitious composition useful for preparing high-resistance cementitious products, obtainable by mixing together a hydraulic binder, finely

ground slag, a fluidifier and/or superfluidifier, a setting regulator, and aggregates characterized as follows:

- (i) the aggregates are made up, for 75-95 wt %, of three highly monogranular fractions (A, B, C), having a characteristic grain diameter increasing progressively from A to B to C;[[.]]
- (ii) the ratio between the characteristic grain diameters of the fractions C and B is comprised between 2.2 and 3.2;
- (iii) the ratio between the characteristic grain diameters of the fractions B and A is comprised between 2.2 and 3.2;
- (iv) the remaining 5-25 wt % portion of aggregates (5-25 wt %) consists of a fourth fraction (D) having a low lower monogranularity than fractions A, B, C; and
- (v) fraction A represents at least 40 wt % of the total aggregates present in the dry premix.